

Pattern blocks in the tread of a tyre

The present invention relates to pattern blocks in the tread of a tyre, comprising a tread layer of one or several rubber materials on the texture of the tyre, and pattern blocks separated from each other by wider grooves in this said tread layer, and fine grooves substantially narrower than the said grooves at least in part of these pattern blocks, each of the fine grooves comprising at least one bend or at least one end within the area of the pattern block.

At present, typically very narrow, differently shaped slits, which are also called fine grooves, capillary slits, or lamellae, are used in the patterning of the tread of tyres in cars, delivery vans and trucks as well as other similar vehicles, which are meant to be used in winter conditions and which thus have to have a good grip both on ice, in snow and in slush. In distinction from grooves in the tread, which separate the pattern segments to work separately independent from each other, the internal slits in the pattern segments are so narrow that the sections of the pattern segment on two sides affect each other during driving. Such slits have been decreed, for example, in the publications EP-0 881 103 A1 and EP-0 125 437 A1, in which it is suggested that long bending slits be used, the shape of the slits being different at different places of the tread thickness. The purpose of the first publication is to make it possible to provide the pattern segments with a large number of slits and to retain the number and length of these slits also as the tyre wears during use. In the latter publication, the shaping of the slits is meant to prevent the tearing of the webs between adjacent slits, which may be caused by deformations in the pattern segments during the use of the tyre.

The publication DE-25 49 668 discloses short hook-shaped slits which are arranged in different positions and which do not extend to the grooves between the pattern blocks, but which are found entirely inside the pattern blocks. The publication DE-2 253 717 discloses also hook-shaped, and additionally V-shaped and zigzag-shaped relatively short slits, of which only one is found in each pattern block according to some applications indicated in the figures of the publication; according to some other applications, several such slits may be included in one pattern block so that they are arranged in line in accordance with the principal direction of the slits or in line transverse to the principal direction of the slits. According to the publication, the several slits in the same pattern block are generally placed at a relatively long distance from each other especially when the line direction of the slits is transverse

to the principal direction of the single slits. In one alternative the slits in the same pattern block are arranged as extensions to each other so that the slits are not in the least overlapping, but their ends are rather close to each other. The influence of the shapes and positions of the slits is not disclosed in the publication, but according to the publication it is essential that the surface pattern contains sections in the circumferential direction of the tyre that differ from each other in relation to the number of the surface profile units and grooves per area unit and/or contour shapes and/or size and/or arrangement. The purpose is here to reduce noise from the tyres and to provide sufficient grip on different road surfaces and in different weather conditions, such as in snow and on ice. Both the treads according to the publication DE-25 49 668 and the publication DE-2 253 717 contain very few, of these slits, i.e. fine grooves, and the suggested surface patterns of the tread do not provide anywhere near the sufficient grip properties according to the present level of requirements.

The object of the invention is to provide such a tread for the vehicle tyre, which provides the tyre with good grip on a road surface with ice, slush, or snow, and which retains these grip properties as well as possible also as the tyre wears out, i.e. the tread becomes thinner. The second object of the invention is to provide such a tread, also the other driving properties of which are good both as new, i.e. unworn, and as worn, even if the rubber material used for the tread were relatively soft, i.e. flexible rubber material.

The problems decreed above are solved and the objects defined above are realised with the tread of the invention as defined in claim 1 and claim 23.

One important advantage of the invention is that each pattern block can be provided with the desired big or relatively big number of slits so that the grip of the tyre can be made excellent, but however so that the sections of the pattern block separated from each other by slits in an unworn tread are kept sufficiently strongly or rigidly together, thus making the driving behaviour of even a new tyre excellent and not too yielding, for example, in the changes of the driving direction, i.e. the tyre is not "sluggish", even as new. Another advantage of the invention is that, as the tyre wears down, for example, the effective number of slits remains at least almost unchanged, i.e. the number or the effective length of the slits is not reduced decidedly or to a harmful extent, so that the grip properties remain good in snow, slush, and on ice. This also provides the tread with a roughening or pilling property continuing substantially until the end of the operating life of the tyre so that points projecting into the small inequalities of the road surface and thus increasing the grip are generated onto the tread.

Figure 11 is a detailed description of the cyclically uneven surface shape of the outer surface of the tread and especially of the nubs according to the invention, separated by slits, in a tyre worn at least to some extent in use, shown as a section perpendicular to the outer surface of the tread, corresponding to the Figs. 9 and 10.

Besides the components not decreed in this specification, the vehicle tyres filled with air comprise, among others, the carcass 25, which nowadays typically contains a radial texture in the area of the tread, and on top of the carcass a tread layer 20 manufactured of one or several rubber materials. This tread layer 20 comprises pattern blocks 1 separated from each other by wider grooves 21, and at least in part of these pattern blocks fine slits 2 or capillary slits or fine grooves or lamellae (the terminology is not completely established) or simply just grooves 2, which are essentially narrower than the said grooves, each of the slits comprising at least one bend 5 or at least one end 4 within the area A1 of the pattern block. The grooves 21, the pattern blocks 1 and the slits 2 form together with possible circumferential ribs 17 the surface pattern of the tread. The tread grooves 21 refer to grooves, the groove depth H3 of which is sufficiently large and the groove width W4 so large that the side edges 19 of the adjacent pattern blocks 1 separated from each other by the groove do not at least to a substantial extent contact each other during the use of the vehicle tyre, i.e. during driving, even during a change in speed and/or direction. Thus, the pattern blocks do not rest on each other more when the tyre is stationary than during accelerations, decelerations or changes in direction, but the pattern blocks can elastically deform at least generally independently, irrespective of the other pattern blocks and their deformation. This can be understood from Figure 9, in which a broken line presents block patterns 1 that have been somewhat deformed elastically, and the groove 21 between them. The groove width W3 of the grooves 21 is generally at least 5 mm or more, when vehicle tyres, especially tyres for cars or delivery vans or trucks are concerned.

Things are different when slits 2 included in the pattern block 1 are concerned, the slit width W2 of these slits being designed so small that the different sections of the same pattern block on the opposite sides of the slit 2 rest on each other during a change in speed and/or direction. In this case, the opposite sides 16a and 16b of each slit 2 in the pattern block 1 come into contact with each other from a smaller or wider area at least during accelerations or decelerations or changes in direction, and thus the sections in the pattern block separated by the slit/slits, in the tread of the invention the nubs 8, support each other in driving situations including changes. During the said changes in speed and/or direction, the nubs 8 in the tread on two

sides of the slit 2 recline in relation to the circumferential surface of the tyre in rest condition, and their outer surfaces 22 form the zigzag-shaped or wavelike form, seen in Fig. 10, thus offering improved grip points to the base, which furthers the grip of the tyre. The slit width W2 of the slits 2 is typically at least about 0.1 mm or at most about 1.5 mm, such as 0.3 mm - 0.8 mm, although even smaller or, for example in truck tyres, wider slits are possible. The possible slit width W2 is influenced by the thickness of the tread, or in other words, the slit depth H3 so that in a tyre with a bigger groove depth, wider slits 2 can be used than in a tyre with a smaller groove depth, because the deflection of the pattern block 1 is bigger with the same force, and thus the sides 16a, 16b of the slit become more easily into contact with each other, even if their distance, i.e. the slit width were bigger when the slit depth H3 is big, as compared with a case in which the slit depth would be smaller.

According to the invention, at least part of the pattern blocks 1 comprises surface tear points 10 between at least two adjacent slits 2. In this specification, the universal reference number 2 is used of the slit in a case when reference is made to the slit in general, and its features are not defined; the specific reference numbers 2a - 2e are used in a case when reference is made to a slit of a certain type. According to the first principle of the invention, each surface tear point 10 is developed from webs 3a, 3b between the end 4 of at least one slit 2 and at least one second slit 2 or its end 4. Alternatively, according to the second principle of the invention, each surface tear point 10 is developed from webs 3c, 3d between the bend of one slit 2 and one second slit 2 or its bend 5. In addition, the web width W3 of the said webs 3a - 3d in the surface tear points 10 is at most five times the slit width W2 of the slit 2a - 2e, and two adjacent slits 2a - 2e further restrict between their mutual webs 3a - 3d within the pattern block 1 nubs 8 with an area A1. Here, the web width W3 refers to the distance between adjacent slits, as can be seen from the Figures. In the surface tear points 10, the webs 3a - 3d also have a web thickness P3, which is a measure perpendicular to the web width W3, based on the projection of the slit width W2 of the slit to the level parallel to the web width at that point. In the embodiment in Figs. 2A, 2C, 2D, 4 and 7, the web thickness P3 is approximately equal to the slit width W2; in the embodiments in Figs. 2B and 3 slightly smaller; in the embodiments of Figs. 5B, 6 and 7A about $2 \times W2 / \sqrt{2}$, if in the bends described later, the slits 2b, 2d form a right angle, and in the embodiments in Figs. 5A and 8, approximately half of the former. Rather generally, although not always, the web thickness is $P3 = W2 / \sin \delta$, in which the angle δ is the angle between the direction of the web width of the slit and the slit coming to it, and double compared with this in a

case, in which several slits come to the surface tear point. If the slits between the surface tear points 10 are straight, the angle $\delta = \alpha$. In the embodiments of Figs. 7B and 7C, the web thickness is approximately equal to the web width W3. It is obvious that the values for the web width W3 and web thickness P3 deviate from the ones told, in a case in which the shape of the slits 2 deviates from the ones shown in the Figures, as can be the case according to the invention.

In the surface tear points 10, the web width W3 and the web thickness P3 are dimensioned according to the rubber material or rubber materials of the tread 20 so that, as the tyre is used during driving, the pier or ridge or web 3a - 3d of the invention tears into a certain depth H1, starting from the respective outer surface 22 of the tread, the tear depth H2 being substantially smaller than the groove depth H3 and the slit depth H2. According to the invention, the tear depth H1 should be at least 0.5 mm and at most 1.5 mm of the outer surface 22 of the tread. Preferably the tear depth H1 is near to 1.0 mm, such as 0.8 mm - 1.2 mm. This tearing of the web 3a - 3d can be understood with the help of Figures 9 and 10. As the pattern block 1 bends due to the influence of the change in speed and/or direction of the tyre, a larger deformation occurs in the section of the height of the pattern block, which corresponds to the slit depth in question at a given time, this section being closer to the outer surface 22 and ending to this outer surface, than in the part of the pattern block which is closer to the tyre carcass 25. In the said section near the outer surface 22 and ending to the outer surface, the dimension of which is the said tear depth H1, a shear stress parallel with the slit depth H2 of the slit 2a - 2e is generated to the web 3a - 3d due to bending, the stress exceeding the tear strength of the rubber material on this restricted area, because of the predetermined relatively small cross section of the web determined by the web width W3 and the web thickness P3. Thus, the tread of the tyre contains also upon wearing out, i.e. as the slit depth H3 and the slit depth H2 decrease, a tear of the web 3a - 3d extending generally always to equally big tear depth H1 from the prevailing outer surface, i.e. the web is in fact removed from the outer surface 22 to the depth H1. On the dimension H4 of the rest of the slit 2a - 2e, the size of which is thus H2-H1, the deformation of the pattern block 1 is smaller, and the shearing force parallel to the slit is thus considerably lower so that the tear strength of the rubber material is not exceeded, but the web remains unbroken. This configuration of the tread of the invention has the special advantage that the grip properties of the tyre tread are completely or almost identical to those of a tread which would contain continuous and fully open slits and between them tilting or bending rubber sections, such as nubs 8 of the invention, etc.; but simultaneously, also the second advantage is achieved that, in the lower part of

the webs, on the dimension H4, the webs further connect the opposite sides 16a and 16b of the slit to each other so that the total rigidity of the pattern block 1 is identical to or at least close to the rigidity of such a pattern block which has no slits, which again reduces the wandering of the tyre during driving. The webs 3a, 3b, 3c, 3d forming the surface tear points thus connect the adjacent nubs 8 to each other from the bottom 23 of the slits 2 towards the outer surface 22 of the tread from the height of the said measure H4, the measure H4 decreasing as the tyre wears out at the same time as also the slit depth H2 decreases. On each wear level of the tyre, the decreasing measure H4 is smaller than the prevailing decreasing slit depth H2. Thus advantageous effects are achieved, which traditionally have been considered as conflicting or excluding each other.

Besides the matters mentioned above, it can be stated about the dimensioning of the said piers or ridges or webs 3a – 3d that the web width W3 is preferably at most four times the slit width W2, or at most two times the slit width. In experimental checks with a certain tyre type it has been found that the tread works in the way referred to above also when the web width W3 of the webs 3a – 3d is substantially equal to the slit width W2. The web thickness P3 of the said webs 3a – 3d again is at most three times the slit width W2 of the slit, or at least half of the slit width. In experimental checks with a certain tyre type it has been found that the tread works in the way referred to above also when the web thickness P3 of the webs 3a – 3d is 0.8x – 1.5x the slit width W2. Reducing the web thickness to be smaller than the slit width requires special design of slits, not decreed in detail here – their local narrowing – in the surface tear points 10. In this case it naturally has to be noted that the dimensioning of the webs 3a – 3d depends of the type of the rubber material for the tread 20, especially on the flexibility and tear strength of the rubber material, and of course of the type and size of the tyre. As the flexibility, i.e. elasticity of the rubber material increases the shearing stress increases, which would require that the webs be made thicker if the tear strength remained unchanged, and in a reversed case, as the elasticity decreases, the shearing stress decreases, which should make it possible to make the webs narrower. In practice, the situation is rather complicated, because most often the elasticity and tear strength of rubber are not independent from each other. At present it is believed that the dimensions determined above are either right or at least indicative, but because of the large number of effective factors and mutual dependence, smaller or bigger deviations may occur. For achieving sufficient symmetry, it is expediently estimated that the web width W3 and the web thickness P3 deviate from each other at most $\pm 50\%$. As the present practical values it can be stated that the web width W3 of the webs is at most 1.5 mm and at least 0.3 mm, or

the web width is preferably 0.5 mm – 1.0 mm and that, respectively, the web thickness P3 of the webs is at most 1.3 mm and at least 0.2 mm, or preferably 0.4 mm – 0.9 mm.

The surface tear points 10 decreed above are thus provided onto the tread of a tyre by arranging to it points with small cross-dimensions, to which the stresses caused by the deformations of the tread and especially of the pattern blocks 1 during driving are directed. When forming these surface tear points it is advantageous to utilise the ends 4 of the slits 2 and/or bends 5 of the slits 2, as will be decreed later in connection with certain forms of embodiment. In the surface tear points 10 it is preferable to use relatively sharp bends 5, as in the figures, for directing the stresses decreed above to a sufficiently restricted area, but also somewhat curved bends 5 may be applied. The said bend 5 is alternatively either the angle $5 = 5a$, the sides of which are formed by the slit, and of which the slit continues as straight or curved sections, or the curve $5 = 5b$, which continues as straight sections, and/or convex and/or concave sections. The reference number 5 refers to the bend in general, and the reference numbers 5a and 5b are only used to individualise the special features of the bend. The design of different bend types will be handled in detail later. At present it is believed to be advantageous that each one of the webs 3a, 3c, 3d forming surface tear points 10 is located on the convex side K1 of the bend 5 in question, as is shown in Figures 2B – 2D, 5B – 5C, 7A and 7C. In this case the surface tearing of the invention occurs between the end 4 of the slit or slits 2 and the convex side K1 of the second slit 2 or the convex side of the bend 5, and likewise between the convex side K1 of the bend 5 of the slit 2 and the convex side K1 of the second slit 2 or the convex side K1 of the bend 5. In the cases of Figures 2A, 3, 4 and 7C, each one of the webs 3a forming surface tear points 10 is located on the straight section of the second slit or slits or approximately on the straight section; and in the cases of Figures 5A – 5B, 7B – 7D and 8, each one of the webs 3b forming surface tear points 10 are located between the ends 4 of the slits, which also are good alternatives. It is also possible to arrange each one of the webs 3a, 3c, 3d forming surface tear points 10 onto the convex side K2 of the bend 5, as is shown in Figure 7D. The surface tearing of the invention occurs then between the end 4 of the slit or slits 2 and the convex side K2 of the second slit 2 or the convex side of the bend 5. It has to be noted that, besides one or several webs of one web type 3a or 3b or 3c or 3d, each one surface tear point 10 may simultaneously have also several webs 3a and/or 3b and/or 3c and/or 3d of different types. Such a surface tear point 10 consisting of a combination of webs of different types is shown in the rightmost web point in Figure 7A and in Figure 7D.

Figures 2A-2D depict solutions of the invention, in which at least two adjacent slits 2 both contain two bends 5, which open substantially to opposite directions in a single slit. Such relatively short, hook-shaped, Z-shaped or S-shaped slits, which do not usually extend across the pattern block between its opposite sides, are here referred to as the slit 2a of the first type. A single slit may naturally extend from its one end to the side 16a or 16b of the groove. In a pattern block, such slits 2a of the first type are additionally found two or several interlaced in row 18 in uniform positions, forming webs 3a of the first type so that the principal directions D7 of the intermediate sections 7 between two bends 5 of a slit are either parallel or gradually changing their direction in a fan-shaped manner. The webs 3a of the first type are formed into points, in which the end 4 of one slit 2a meets the bend 5 or an intermediate section 7 of the adjacent slit 2a, i.e. some other point than the end, on the web width W3. The row 18 refers also to the row of nubs 8 in the pattern block 1. The principal directions D7 of the said intermediate sections 7, which may be straight, as in Figures 2A and 2B, or curved, as in Figures 2C and 2D, or bending, form the angle of deflection α in relation to the constant row direction D1 of the row, as in Figures 2A, 2B and 2D, or in relation to the changing local row direction D1, as in Figure 2C. The angle of deflection α may have the angular value of 30° - 90° . The row direction D1 is formed of an envelope or direct envelope, which travels through the successive surface tear points 10 corresponding to each other in the row 18, and which is identical to or parallel with the envelope passing through the middle points of successive nubs 8 in the row 18. This determination of the row direction D1 concerns all row directions mentioned in this specification. In the case of Figures 2A-2D, the envelopes passing through the surface tear points and the middle points of the nubs are united.

In Figure 3 there is shown a solution of the invention, in which at least two adjacent slits 2 both contain one bend 5. Such L-shaped or V-shaped relatively short slits, which do not usually extend across the pattern block between its opposite sides, are here referred to as the slit 2b of the second type. In a pattern block, such slits 2b of the second type are found in pairs in the row 18, the slits 2b of the second type being found interlaced in the said slit pairs 11 and forming mirror-like webs 3a of the first type, in which the end 4 of one slit 2b meets the bend 5 or intermediate section 7 of the adjacent slit 2b on the web width W3. The intermediate section 7 may be either curved or bending or, as in Figure 3, straight. In the case of Fig. 3, the envelopes passing through the surface tear points 10 and the middle points of the nubs 8 unite forming the row direction D1.

Figure 4 presents a solution of the invention, in which at least two adjacent slits 2 both contain two bends 5, which open principally to the same direction in a single slit. Such U-shaped or [-shaped or {-shaped relatively short slits, which do not usually extend across a pattern block between its opposite sides, are here referred to as the slit 2c of the third type. In a pattern block, such slits 2c of the third type are arranged alternately interlaced and mirror-like in the row 18, thus forming webs 3a of the first type already defined above. In the slits 2c, the average directions D7 of the intermediate sections 7 between two bend points are parallel with each other and with the constant row direction D1 of the row. The intermediate section 7 may be either curved or bending or, as in Fig. 4, straight. In the case of Fig. 4, the envelopes passing through the surface tear points 10 and the middle points of the nubs 8 unite forming the row direction D1.

In Figures 5A-5B there is shown a solution of the invention in which at least two adjacent slits 2 both contain one bend 5, so that this concerns the slit 2b of the second type already decreed earlier. In a pattern block, such slits 2b of the second type are arranged in pairs in row, the slits 2b in the slit pairs 12 being arranged mirror-like opposed, forming – in a case in which the bends 5 in slit pairs 12 open towards each other, as in Fig. 5A – webs 3b of the second type, and/or – in a case in which the bends 5 in slit pairs 12 open away from each other, as in Fig. 5B – webs 3c of the third type. The webs 3b of the second type are formed as the ends 4 of two slits meet each other on the web width W3, and the webs 3c of the third type are formed as the bends 5 of two slits meet each other on the web width W3. The slit pairs 12 with their webs 3b or 3c form the row 18, and additionally, the said web width W3 is located between the ends 4 of the slits in the successive slit pairs 12 of the row 18 so that web combinations 9 between the slit pairs, as in Fig. 5B, or webs 3b of the second type, as in Fig. 5A, are generated. In the web combinations 9, two webs 3b of the second type thus meet each other on the web width W3 so that the web combination 9 is in a way a combination of four webs, in which web widths W3 are found at least in two directions transverse or perpendicular to each other. In the case of Figures 5A and 5B, the envelopes passing through the surface tear points 10 and the middle points of the nubs 8 unite forming the row direction D1.

Figure 6 presents a solution of the invention, in which at least two adjacent slits 2 both contain three or several bends 5, which open alternately to substantially opposite directions. Such zigzag-shaped or wavelike relatively long slits are here referred to as the slit 2d of the fourth type. In a pattern block, such slits 2d of the fourth type are arranged rectilinearly in pairs, the slits in the slit pairs 12 being arranged op-

posed and mirror-like so that every other of the opposed bends 5 opening away from each other are found at a distance of the web width W3 from each other, forming webs 3c of the third type. The bends 3c of the third type are thus formed between the convex sections of the bends 5, as in Figures 5B, but deviating from this, the slits 2d of the fourth type continue with bends 5 opening to opposite directions. The webs 3c are found in the row 18 corresponding to the principal direction of the slits. In the case of Figure 6, the envelopes passing through the surface tear points 10 and the middle points of the nubs 8 unite forming the row direction D1.

In Figures 7A-7C there is shown a solution of the invention, in which at least one of two adjacent slits 2 is either the slit 2b of the second type containing one bend point opening towards another slit, as in Figs. 7B and 7C, or the slit 2d of the fourth type containing three or several bend points, opening alternately substantially to opposite directions, as in Fig. 7A; and the other slit 2e of the fifth type is substantially straight and continuous, as in all the Figures 7A-7C. The slit 2e of the fifth type does not need to be linear, but it may be evenly curving, such as a section of a circle, ellipse, parabola, etc., or some other free arched shape; or it may also possibly be wave-form, as long as it is substantially less and more gently bending than the adjacent slit 2b, 2d of the second or fourth type. Here is thus a slit pair formed by the substantially straight slit 2e of the fifth type and the slit 2b of the second type, which has been decreed earlier, or by a number of slits; or a slit pair formed by the substantially straight slit 2e of the fifth type and the bending slit 2b of the fourth type, which has been decreed earlier. Thus, there are two alternatives for the webs. First, the ends 4 of the slit or slits 2b of the second type are found at a distance of the web width W3 from the slit 2e of the fifth type, forming webs 3a of the first type, as has been decreed earlier. If the distance of the successive webs of the first type on the measure of the slit 2e of the fifth type corresponds to the web width, web combinations 9 are formed also in this case, as in Figures 7B and 7D. Secondly, the bends 5 of the slit of the fourth type are found at a distance of the web width W3 from the slit 2e of the fifth type, forming webs 3d of the fourth type. The webs 3d of the fourth type are thus formed as the bends 5 meet the substantially straight slit 2e on the web width. Both the webs of the first type and the webs of the fourth type 3a, 3d form the row 18. In the case of Figures 7A-7C, the envelopes passing through the surface tear points 10 and the middle points of the nubs 8 do not unite, but they are parallel in relation to each other and to the slit 3e of the fifth type, forming the row direction D1.

Figure 8 presents a solution of the invention, in which at least two adjacent slits comprise four principally straight slits 2e of the fifth type. Here both the slits adjacent to each other consist of the combination of two single slits. In the combination of two adjacent slits, the first ends 4 = 4a of the slits of the fifth type lie at a distance of the web width W3 from each other, forming first webs 3b = 3b₁ of the second type. Further, the slits 2e of the fifth type are found in pairs 13 in row so that their second ends 4= 4b extending away from the said first webs 3b₁ of the second type lie at a distance of the web width W3 from each other, forming second webs 3b = 3b₂ of the second type. In the row 18 between the first webs 3b₁ of the second type of the successive slit pairs 13 there further is the said web width W3 so that web combinations 9 are formed with the third webs 3b = 3b₃ of the second type. Also in this case, the web combination 9 is in a way a combination of four webs in which web widths W3 are found at least in two directions transverse or perpendicular to each other, just as in the surface tear points corresponding to Figure 5A. The first webs 3b = 3b₁ of the second type form the row 18. In the case of Figure 6, the envelopes passing through the surface tear points 10 and the middle points of the nubs 8 unite forming the row direction D1. Also in this case, the reference number 3b refers to the web of the second type in general, and the more individualised reference numbers 3b₁, 3b₂ and 3b₃ refer to webs of the same type in different points only for improving the understandability.

For achieving sufficient effect, each pattern block 1 contains at least one row 18 of surface tearing points 10 formed by the webs 3a-3d, and thus nubs 8 restricted by slits 2 between them. Each row contains at least two nubs 8. However, it is more preferable to provide the pattern blocks 1 with two or several said rows 18, each of which contains two or several nubs 8. Thus, the pattern block 1 contains preferably altogether at least five nubs 8. The row direction D1 of the rows 18 determined above is transverse to the circumferential direction Tc of the tyre, and preferably, the row direction forms the row angle K2 90° and 45° to the circumferential direction, as can be seen from Figure 1. The nubs have the essential length L1 and width W1 both in the circumferential direction Tc of the tyre and in the lateral direction Tw of the tread. Further, the said nubs 8 are found in pattern blocks in the shoulder areas Ts of the tyre and in pattern blocks in the direction of the middle parts Tm of the tyre from them, such as in the circumferential rib 17 or ribs of the tread, as in the example in Figure 1. The circumferential webs, such as the middle web, can naturally be left without the slits 2a-2e of the invention and without the nubs 8 of the invention. The nubs 8 of the invention, which are in a manner explained above, attached to the adjacent nubs 8 or the other adjacent section of the pattern block

with the measure $H4 = H2 - H1$ of the webs 3a-3s changing along with the wearing down of the tyre, work forming the outer surface 22 of the pattern block uneven as the pattern block 1 and the nubs 8 decline, as has been decreed earlier in connection with Figure 10. Further, during the use of the tyre, the nubs 8 wear out more strongly from their edges 14, indicated as dot ticks in Figures 2C, 2D, 6, 7C and 8, than from their middle sections, thus generating a structure of the outer surface 22 of the tread deviating locally from the level or an even arc, i.e. an uneven or wave-like structure, which is believed to be a reason for that the tread of the invention has excellent grip also when worn out. This locally or cyclically uneven structure of the outer surface 22 of the tread is shown in Figure 11.

Because the pattern blocks 1 have several nubs 8 of the invention, the area A2 of each nub is thus substantially smaller than the area A1 of the pattern block 1, for example, one third, one fourth or one fifth, or an even smaller share of the area A1 of the pattern block. However, the nubs 8 have to be larger than a certain minimum size both from their area and both dimensions perpendicular to each other in the direction of the outer surface 22. The nubs have to be of such a size and shape that the biggest possible circle to be fitted into or drawn onto the outer surface 22 in the area of slits 2 and surface tear points 10 restricting it, i.e. the circle Y found on the area A2 of the nub and touching the slit 2 restricting it at least in three points – if the nub is restricted by substantially straight slits – or at least in two points – if the nub is restricted by substantially curved slits – has an area A3 which is at least 1.7 mm^2 , but preferably at least 3 mm^2 , and typically $5 \text{ mm}^2 - 12 \text{ mm}^2$, when tyres of a car are concerned. According to the invention, both measures L1, W1 of the nub perpendicular to each other in the direction of the outer surface 22 do not advantageously deviate too much from each other, but the total area A2 of the nub is preferably at most four or three times the area A3 of a maximum-sized circle drawn inside the nub, or typically at most double compared with the area A3 of the circle, i.e. $A2 \leq 4 \times A3$, or $A2 \leq 4 \times A3$, or $A2 = 1 \times A3 - 2 \times A3$. In tyres of a delivery van, the minimum size of nubs 8 is about 1.5 times the values for the car tyres, etc., i.e. the area A3 of a maximum-sized circle Y drawn inside the nubs is at least 2.5 mm^2 or at least 5 mm^2 or $7 \text{ mm}^2 - 24 \text{ mm}^2$, and respectively, the total area of the nubs relates to this area of the circle as above, i.e. $A2 \leq 4 \times A3$, or $A2 \leq 4 \times A3$, or $A2 = 1 \times A3 - 2 \times A3$. In tyres of a truck or a bus, the area of the maximum-sized circle Y drawn inside the nubs is about double the values for car tyres, i.e. A3 is at least 3 mm^2 or at least 8 mm^2 or between 15 mm^2 and 50 mm^2 , and further respectively, the total area of the nubs relates to this area of the circle as above, i.e. $A2 \leq 4 \times A3$, or $A2 \leq 4 \times A3$, or $A2 = 1 \times A3 - 2 \times A3$. The maximum size of the nub 8, or the area A2, depends on

the size of the tyre, being about 40 mm² in car tyres, about 60 mm² in delivery can tyres, and about 100 mm² in truck tyres.

In cases, in which the said bend 5 of the slits is the angle 5a, its angular value β , i.e. the angular space of the slit sections coming to the angle 5a, is at least 60° and at most 120°, and preferably, the angular value β for the said angle 5a is 80° - 100°. The radius of curvature R3 for the said angle 5a is at most three times the slit width W2 of the slit ($R3 = 3 \times W2$) so that it is suitable to be used as a part of the web 3a, 3c and 3d forming the surface tear point 10. It is also naturally possible to form the angle 5a with a smaller radius of curvature, such as $R3 = 2 \times W2$ or $1 \times W2$. Alternatively, the said bend 5 of the slits 2 is an arc 5b curving with a relatively large radius of curvature, which extends – in cases, in which the arc 5b continues as sections 15a with an unchanged radius of curvature R1 – as a single shape to the first curvature χ_1 , the value for which is at least 150° and at most 210°, or preferably 170° - 190°. Alternatively, the arc 5b extends – in cases, in which the arc 5b continues as substantially straight sections 15b – to the second curvature χ_2 , the value of which is at least 60° and at most 120°, or preferably 80° - 100°. Alternatively, the arc 5b extends – in cases, in which the arc 5b continues as sections 15c, the radii of curvature R2 of which are bigger than the radius of curvature R1 of the said arc 5b – to the third curvature χ_3 , the value for which is between the said first and second curvature χ_1, χ_2 .

The fine grooves or slits 2a and/or 2b and/or 2c and/or 2d and/or 2e may extend to the one edge 19 or to two opposite edges 19 of the pattern block 1 and open into the grooves 21 between the pattern blocks in these points. These edges 19 of the pattern block, into which the slits 2 possibly extend, are either parallel with the circumferential direction Tc of the tyre, or they form at most the angle $K1 = 45^\circ$ in relation to this.

The surface tear points 10 of the invention and the webs 3a-3d between the slits 2, or capillary slits, or fine grooves, generating these, may be used in treads of vehicle tyres of any type, irrespective of the shapes of the surface pattern. Of these different tread designs, the surface pattern in Figure 1 is only one example, and the invention is not restricted to this. Likewise, the designs of the slits 2 and the types of the webs may vary within wide ranges and deviate from the ones shown in the Figures.